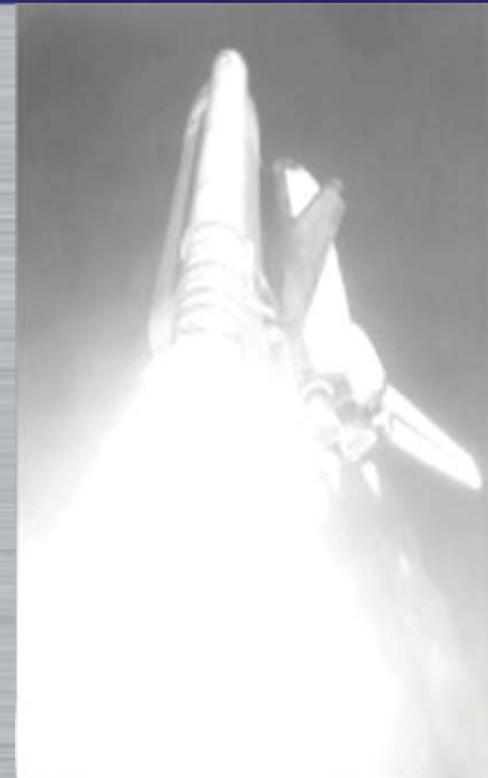


# ARE WE LEARNING FROM PAST PROGRAMS?

ARE WE APPLYING LESSONS LEARNED ?

Bo Bejmuk



# EXAMINE SELECTED SHUTTLE LESSONS LEARNED AND THEIR UTILIZATION IN CONSTELLATION

- **STRUCTURES AND LOADS ANALYSES**
- **AVIONICS**
- **DESIGN FOR OPERATIONS**
- **MARGIN MANAGEMENT**

## PRVIDE CONCLUSIONS

# OUTLINE

- **Introduction**
- **System Integration Approach**
- **Liftoff and Ascent Aerodynamics**
- **Structures**
- **Ascent Flight Control System**
- **Day-of-Launch I-Loads Evolution**
- **Avionics Architecture**
- **Main Propulsion**
- **Software**
- **Lightning**
- **Flight Instrumentation**
- **RCS Thrusters**
- **Materials and Processes**
- **Risk Management**
- **Operational Cost Drivers**
- **Margin Management**
- **Significance of Lessons Learned**
- **Other Applicable Lessons Learned**
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**Lessons learned from  
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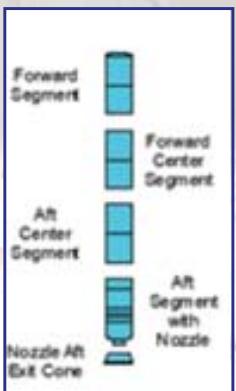
# Introduction

- **Two types of Shuttle Program Lessons Learned are addressed**
  - **Problems – How they were resolved and their applicability to Ares I**
  - **Success Stories – How they were achieved and their applicability to Ares I**
- **Lessons Learned are presented at a fairly high level**
  - Each can be expanded to any desired level of detail
- **Top-level Lessons Learned from Zenit Derived Launch Systems – Sea Launch are included**

# Shuttle Elements



## Ground Systems

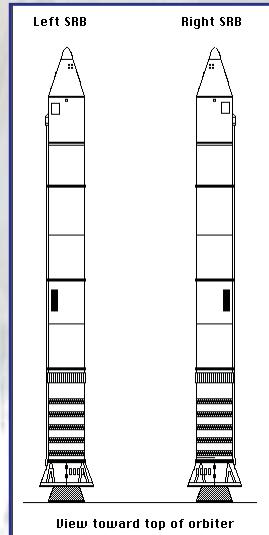


## Solid Rocket Motor (SRM)

1/20/2012



External Tank



Solid Rocket  
Boosters (SRB)



Shuttle System  
Main Engines



Orbiter\*

\* Two cargo configurations analyzed – 65K lbs and 0 lbs payloads

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# STS-1 SRB Ignition Overpressure (IOP)

## Problem

- SRB IOP measured at the vehicle exceeded the 3-sigma liftoff design environment
  - Accelerations measured on the wing, body flap, vertical tail, and crew cabin exceeded predictions during the liftoff transient
  - Support struts for the Orbiter's RCS oxidizer tank buckled
- Post flight analysis revealed that water spray designed to suppress SRB IOP was not directed at the source of IOP
  - Source of IOP was believed to be at the plume deflector
  - STS-1 data analysis showed the primary source located immediately below the nozzle exit plane
- Tomahawk ignition transient used for preflight characteristics were very different from that of the SRB

# STS-1 SRB IOP (Continued)

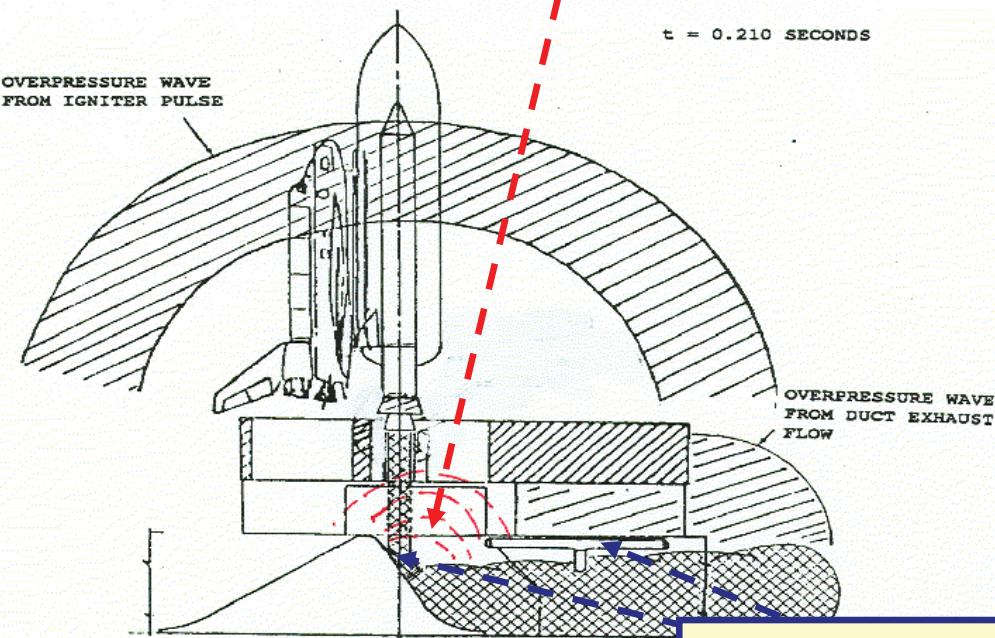
## Corrective Actions

- Solution to the SRB IOP was treated as a constraint to STS-2
- IOP “Wave Committee” organized with participation of the NASA and the contractors
- A 6.4% model was modified to allow simulation of simultaneous ignitions of two SRBs with the firing of one motor only
  - Add a splitter plate in the flame bucket
- A new scaling relation was developed based on blast wave theory
- A series of 6.4% scale model tests were conducted to evaluate various concepts of IOP suppression schemes
- Final fixes
  - Redirected water spray for SRB IOP suppression toward the “source” of SRB IOP (Figure 1)
  - Installed water troughs in the SRB exhaust duct
  - Very significant IOP reduction was achieved (Fig. 2)



# Figure 1: STS-1 and STS-2 SRB IOP Suppression Configuration

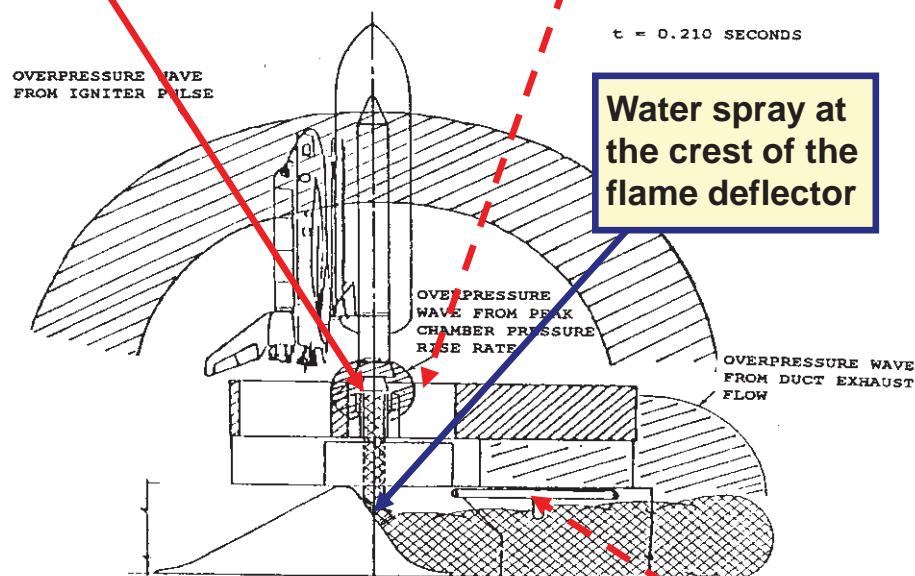
Water spray for STS-1 was designed for IOP  
Source at flame deflector



STS-1 Configuration

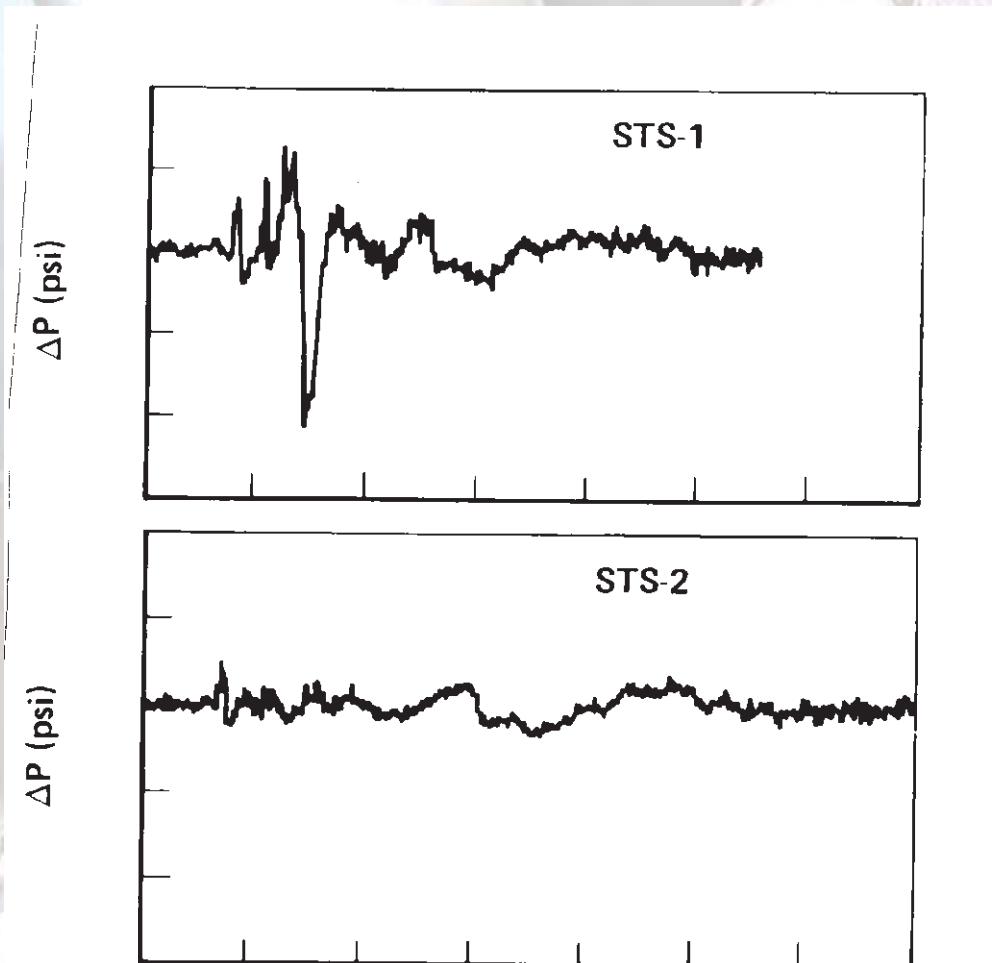
100,000 GPM of water injected into the SRB exhaust beneath the nozzle exit plane

Water troughs cover the SRB duct inlet



STS-2 Configuration

**Figure 2: An overall factor of 5 reduction for the primary IOP waves was achieved with the redesigned system prior to STS-2**



# STS-1 SRB IOP (Continued)

## Lessons

1. SRB Ignition is a powerful driver in liftoff environments
2. System Integration, responsible for liftoff environment definition, accepted the Tomahawk ignition test as a sufficient simulation of SRB ignition IOP – Did not fully appreciate the effect of the differences between the SRB and the Tomahawk ignition characteristics
3. SRB ignition transient for Ares I should benefit from post STS-1 efforts on the Space Shuttle
  - MLP configuration should be evaluated to account for a single SRB
  - If the SRB propellant shape or type is changed, the effect on IOP should be re-evaluated

# **DIRECT BENEFIT TO ARES LIFTOFF**

- **BROAD INVOLVEMENT OF STRUCTURES/AERO COMMUNITY DURING SHUTTLE DEVELOPMENT- CONTINUITY OF MSFC INVOLVEMENT**
- **UTILIZATION OF LEGACY HARDWARE IN ARES FIRST STAGE**

# Ascent Aerodynamics

## Problem

- Plume simulation used during the preflight wind tunnel test program was not adequately implemented
  - Observed significant wing lift and vehicle lofting in STS-1
    - Measured strains showed negative structural margins
- Under-predicted ascent base pressures (base drag over-predicted)
  - Temperature effects were not modeled in cold jet plume simulation parameters used during testing

## Corrective Actions

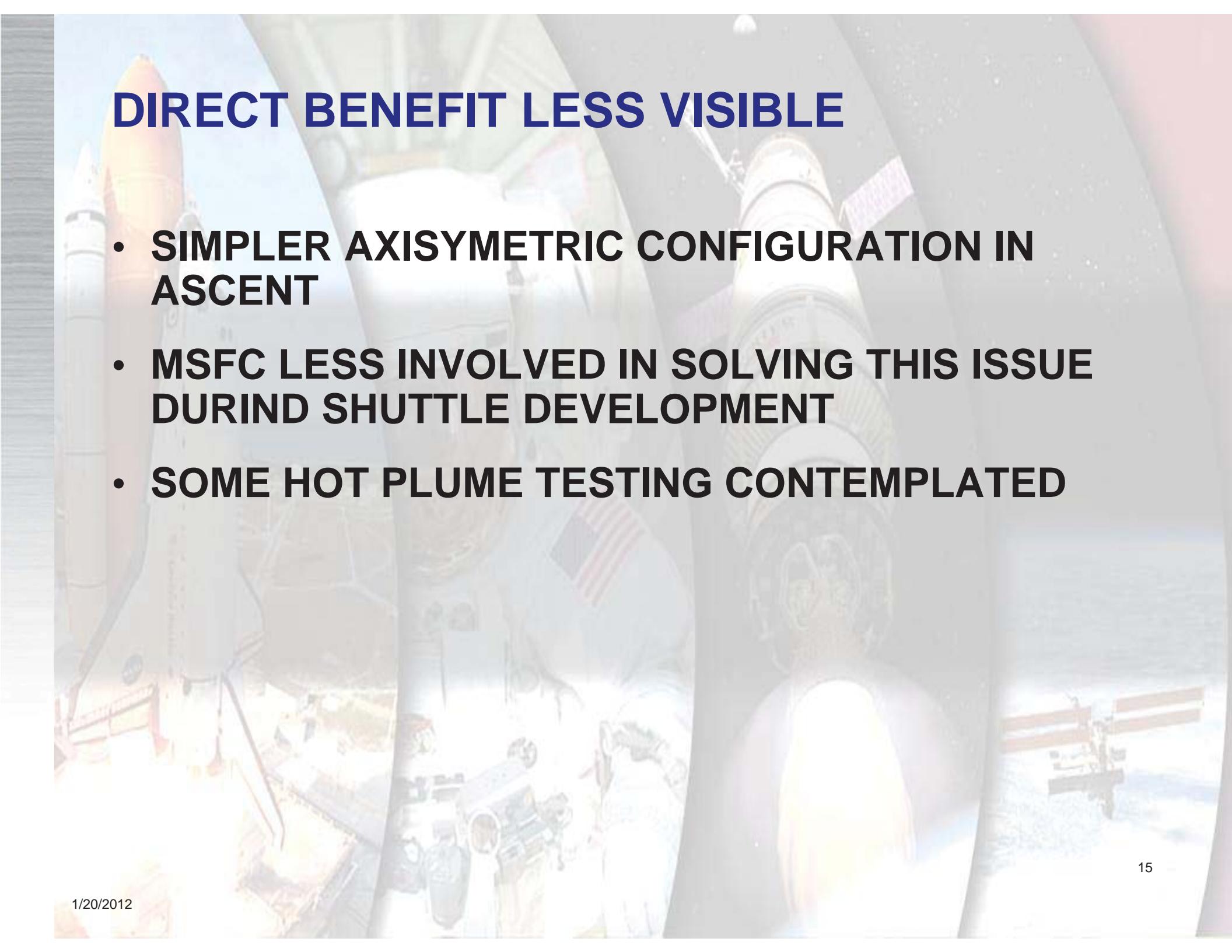
- The Post-flight tests using hot plume simulations improved base and forebody pressure predictions
- The ascent trajectory was changed to a flight with a greater negative angle of attack through High Q
  - The negative angle reduced wing lift
  - The negative angle had to be evaluated for Orbiter windows and the ET side wall pressures

# Ascent Aerodynamics (continued)

## Lesson

- Although the hot plume re-circulation effect is less significant on an axis-symmetric vehicle, it should be accounted for when defining pressure on the base and aft portion of the vehicle

# **DIRECT BENEFIT LESS VISIBLE**



- **SIMPLER AXISYMETRIC CONFIGURATION IN ASCENT**
- **MSFC LESS INVOLVED IN SOLVING THIS ISSUE DURING SHUTTLE DEVELOPMENT**
- **SOME HOT PLUME TESTING CONTEMPLATED**

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# Structures

## Problem

- **Throughout Shuttle development and the initial years of operations many costly structural modifications had to be made to maintain the required 1.4 structural safety factor**
  - The Shuttle structure was designed for a 1.4 safety factor with no additional margin to accommodate changes occurring during the development phase

## Corrective Actions

- As mathematical models and definitions of the environments matured, resulting changes required many hardware changes to eliminate areas of negative margin (below a 1.4 safety factor)
  - These hardware modifications were expensive and time consuming. Additionally, they increased workload at the launch site
  - This tedious activity ensured safe flights and compliance with the safety factor requirement, however it created a significant impact on Shuttle operations

# Structures (continued)

## Lessons

- **If development time is short, structural margin management could be pursued to avoid costly hardware changes as loads analyses mature**
  - A suggested approach could be as follows:
    - Assign additional factor to be applied to the design loads for environments with the greatest uncertainties
      - For example, gravity and pressure loads could have a factor of 1.0 but dynamic and aero loads could have a factor of 1.2
      - All factors would converge to 1.0 as a function of program maturity
    - A method of structural margin management could minimize costly hardware redesign, and program stand downs, but it may result in a somewhat heavier vehicle

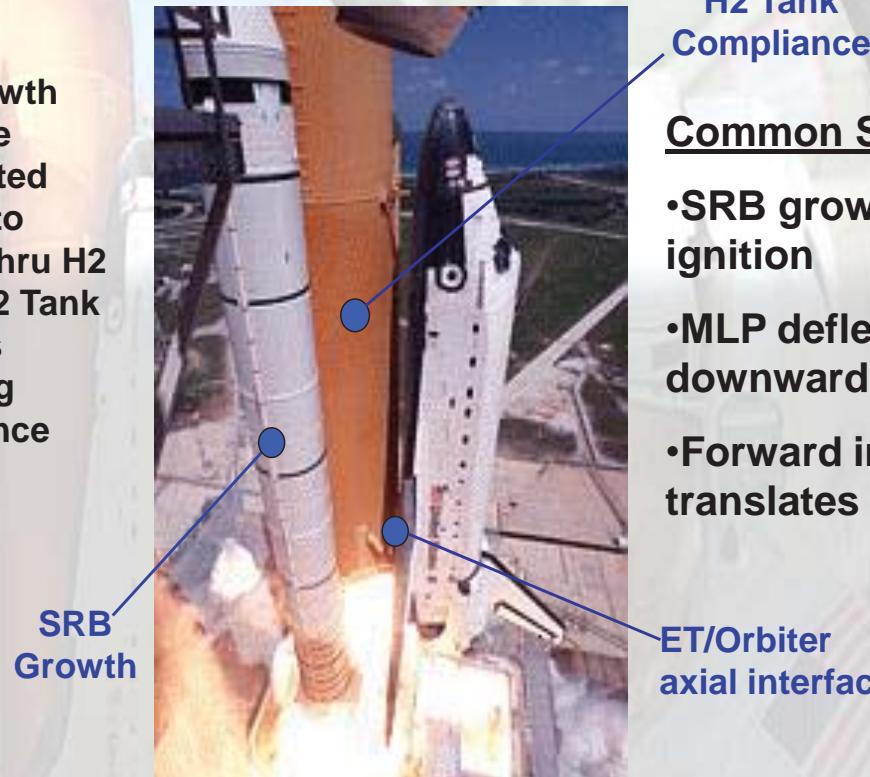
# STRUCTURAL MARGIN MANAGEMENT

- ARES IMPLEMENTED STRUCTURAL MARGIN MANAGEMENT
- ORION IS CHALLENGED BY MASS ISSUE-  
DIFFICULT TO HAVE ROBUST STRUCTURAL MARGIN MANAGEMENT-MASS GROWTH ALLOWANCE STILL IMPLEMENTED

# Liftoff Loads Analyses

SRB growth loads are transmitted directly to Orbiter thru H2 Tank. H2 Tank provides softening compliance

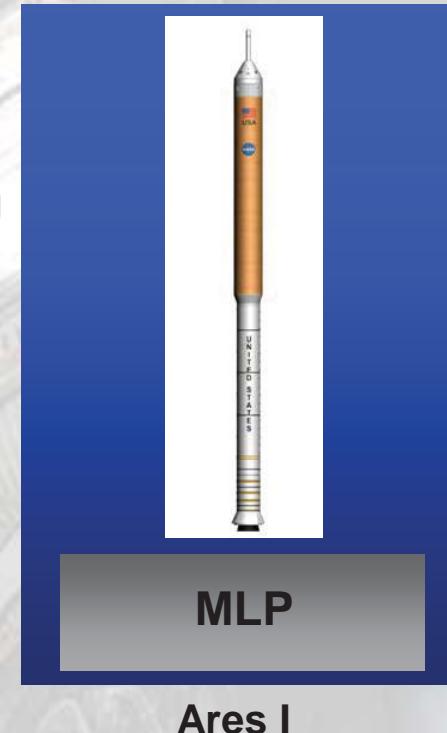
Shuttle



H2 Tank  
Compliance

## Common Shuttle/Ares I

- SRB grows 0.9" during ignition
- MLP deflects downward
- Forward interface translates upward



SRB growth loads are transmitted directly to 2<sup>nd</sup> stage potentially creating more sever L/O loads

## Problem

- Shuttle liftoff (L/O) loads were very difficult to analyze
  - Configuration complexity
  - SRB Ignition Overpressure
  - “Twang” during the SSME thrust buildup
- Vandenberg experience showed that loss of the MLP compliance significantly increased L/O loads
- Flexible washers were planned to restore compliance and avoid vehicle redesign

# Liftoff Loads Analyses (continued)

## Corrective Actions

- SRB ignition delayed until the SRB bending moment (due to SSME thrust buildup) was at zero
- Four independent support posts modeled in L/O simulations
- Monte Carlo method was incorporated
- Ground wind restrictions were implemented

## Lesson

- In spite of the relative configuration simplicity of the Ares I, L/O loads may be a significant design issue due to direct load path between the SRB and the upper stage

# **ARES/ORION LIFTOFF ANALYSES BENEFITED FROM SHUTTLE EXPERIENCE**

- MSFC INVOLVED IN LIFTOFF LOADS  
RESOLUTION – CONTINUITY OF KNOWLEDGE**
- SENSITIVITY TO MLP STIFFNESS**
- EXPERIENCE IN MODELING SRB IGNITION  
FORCING FUNCTION**

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# Day-of-Launch I-Loads Update (DOLILU) Evolution

## Problem

- The launch probability predictions for early Shuttle flights was less than 50%
  - More than half of the measured winds aloft violated the vehicle's certified boundaries

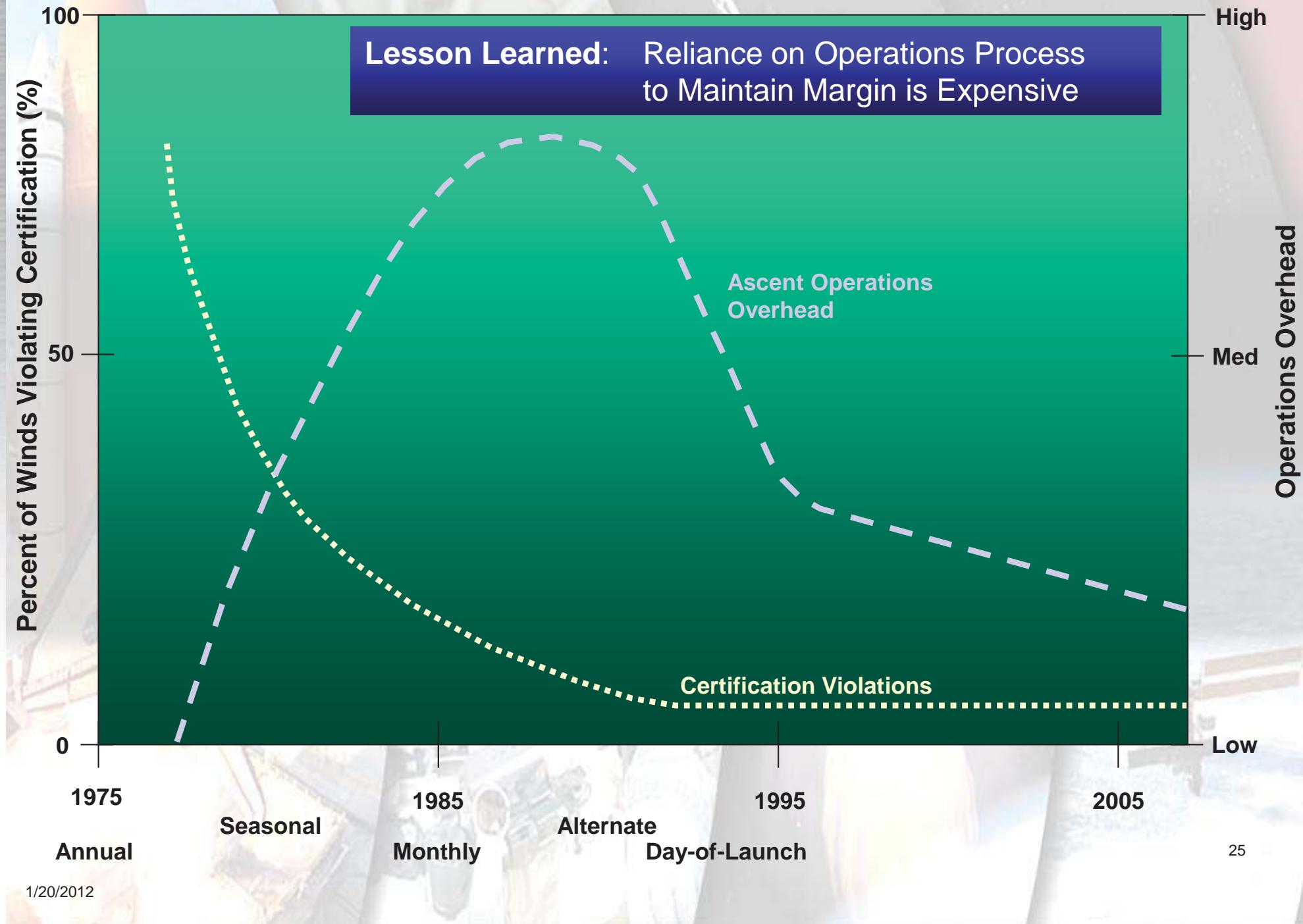
## Corrective Actions

- System Integration led the evolution from a single ascent I-load, through seasonal I-loads, alternate I-loads, and finally arriving at DOLILU
- This process extended over a 10+ year period (Figure 3)
- Concurrently the Program executed 3 load cycles (Integrated Vehicle Baseline Characterization - IVBC) combined with hardware modifications to expand vehicle certified envelopes (Figure 4)
- Current launch probability is well in excess of 95%

## Lesson

- Commit to a DOLILU approach during early development
  - Significantly improves margins

# Figure 3: Ascent Design Operations Evolution



# DAY OF LAUNCH I-LOADS METHODOLOGY IS STATE OF THE ART TODAY

- PLANNED FOR CONSTELLATION ASCENT FLIGHTS
- WINDS ALOFT WILL HAVE LESS EFFECT ON STRUCTURAL WEIGHT
- MORE ROBUST VEHICLE

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# Avionics Architecture

## Problem

- Prevention of loss of vehicle/crew or mission due to avionics failures considering mission duration up to approximately 12 days

## Actions

- Dissimilar solutions (primary, backup and two fault tolerance in avionics hardware/software)
- Establishment of SAIL – Simulation of hardware/software interaction
- Four LRU Mid Value Select (MVS) implemented with appropriate cross strapping to ensure two fault tolerance
- The Redundancy Scheme was required to be test verified
- Two fault tolerance became an avionics system “mainstay” on the Shuttle Orbiter

## Lesson

- The Orbiter system provided a reliable avionics system. For a short duration, missions such as Ares I ascent suggested a tradeoff to be performed between one and two fault tolerance. Overall system reliability could be used in the evaluation.

# Avionics Architecture (Continued)

- Establishing the Fault Tolerance Requirements is a Primary Avionics Cost Driver



**High Time Exposure** ← → **Low Time Exposure**

- Trade off study suggested: One vs. two fault tolerance on Booster
- A “tailored” level of fault tolerance could emerge as the best solution

- The Shuttle approach of two fault tolerance\* was robust, but may be excessive for a boost only vehicle. The overall system reliability (for example 0.999) should drive redundancy requirements.

\* With some compromises



# **CONSTELLATION IS USING “TAILORED APPROACH”**

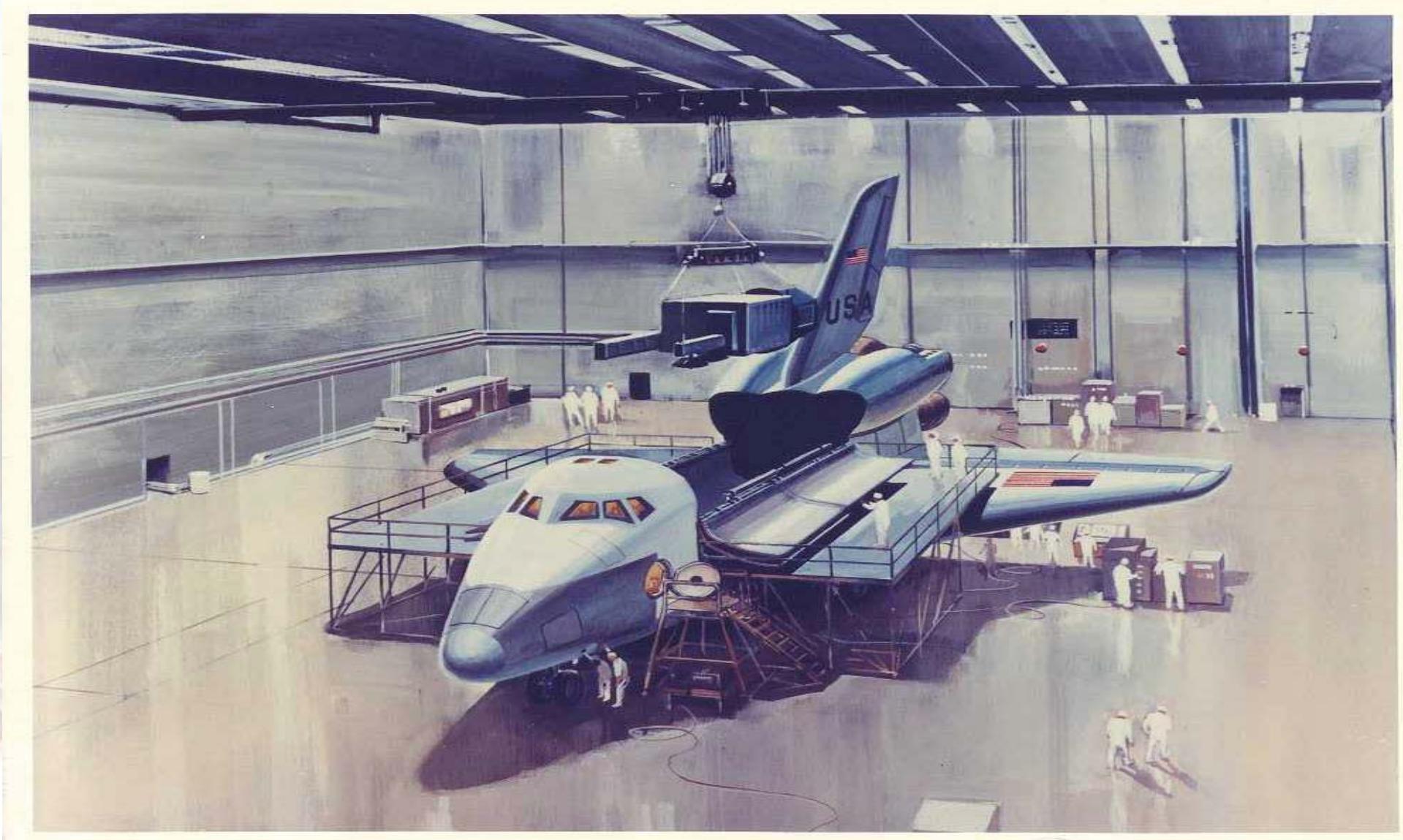
- LOC/LOM DRIVES REDUNDANCY
- ORION MASS/ARES PERFORMANCE ISSUE CONSTRAINS REDUNDANCY
- SOME CONCERNS ABOUT ROBUSTNESS OF AVIONICS
- LIMITED REDUNDANCY EXPECTED TO INCREASE LIFE CYCLE COST

# OUTLINE

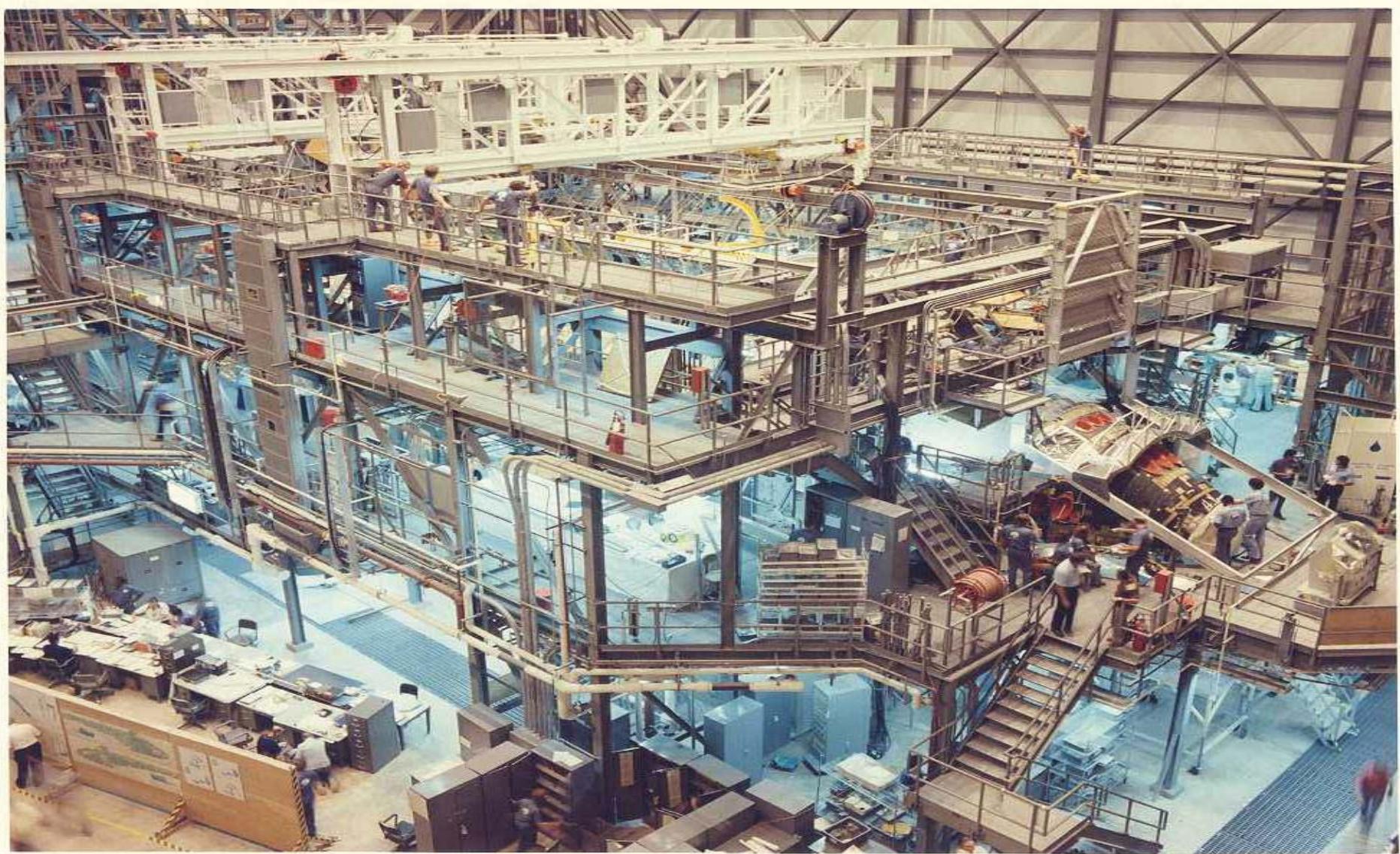
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# Initial Naive Concept of Operations



# Operational Reality



NASA, KSC Photo, dated September 25, 1979, index number "KSC-79PC-500"

# Operational Cost Drivers

## Problem

- **Insufficient definition of operational requirements during development phase**
  - Concentration on performance requirements but not on operational considerations
  - Shuttle design organizations were not responsible for operational cost
  - Very few incentives for development contractors

## Corrective Actions

- **Very labor intensive (high operational cost) vehicle was developed and put into operations**

## Lesson

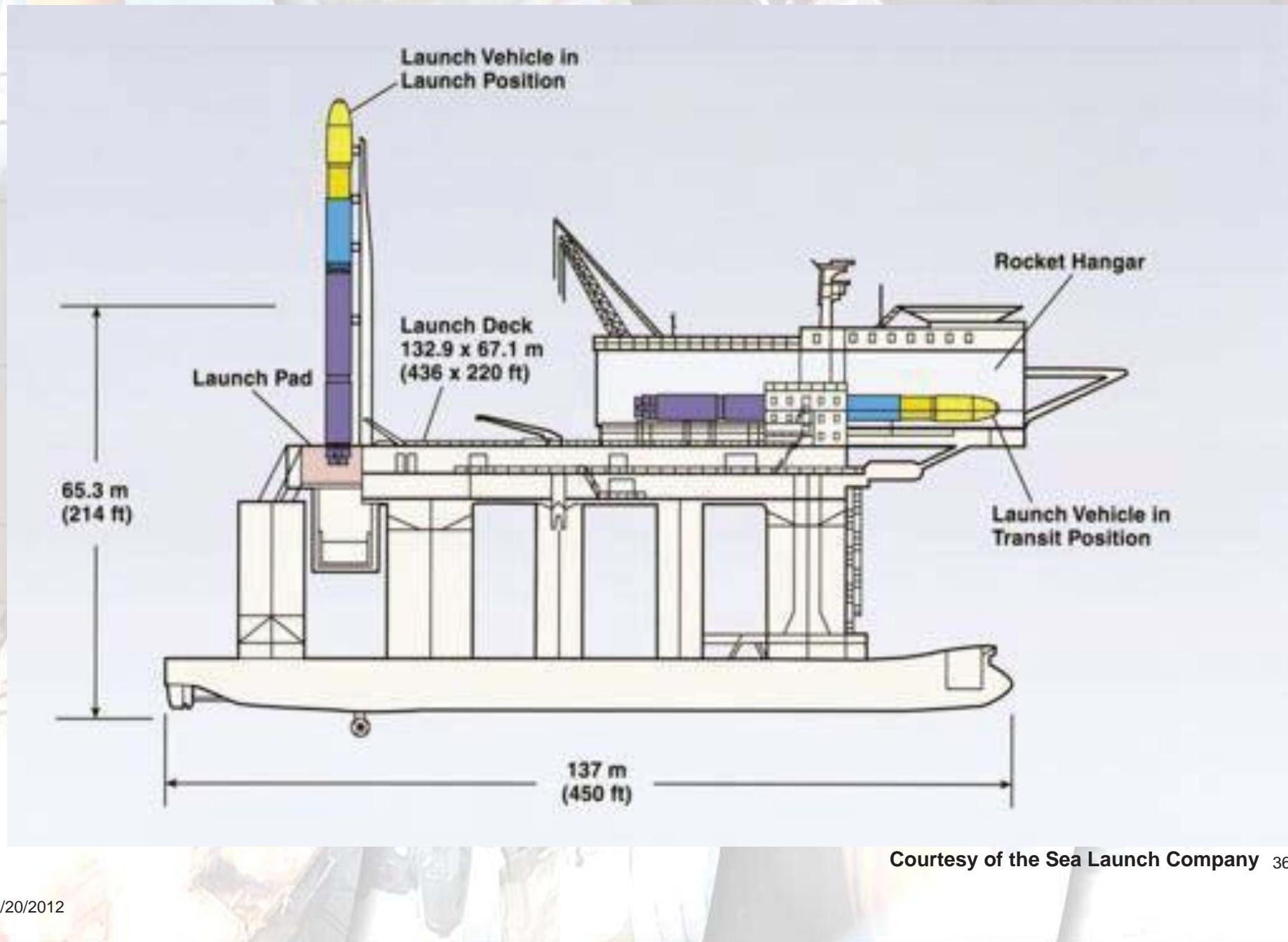
- **Must have the Concept of Operations defined**
- **Levy the requirements on contractors to support the Concept of Operations**
- **Must have continuity and integration between designers, ground operations, and flight operations requirements during the developmental phase**

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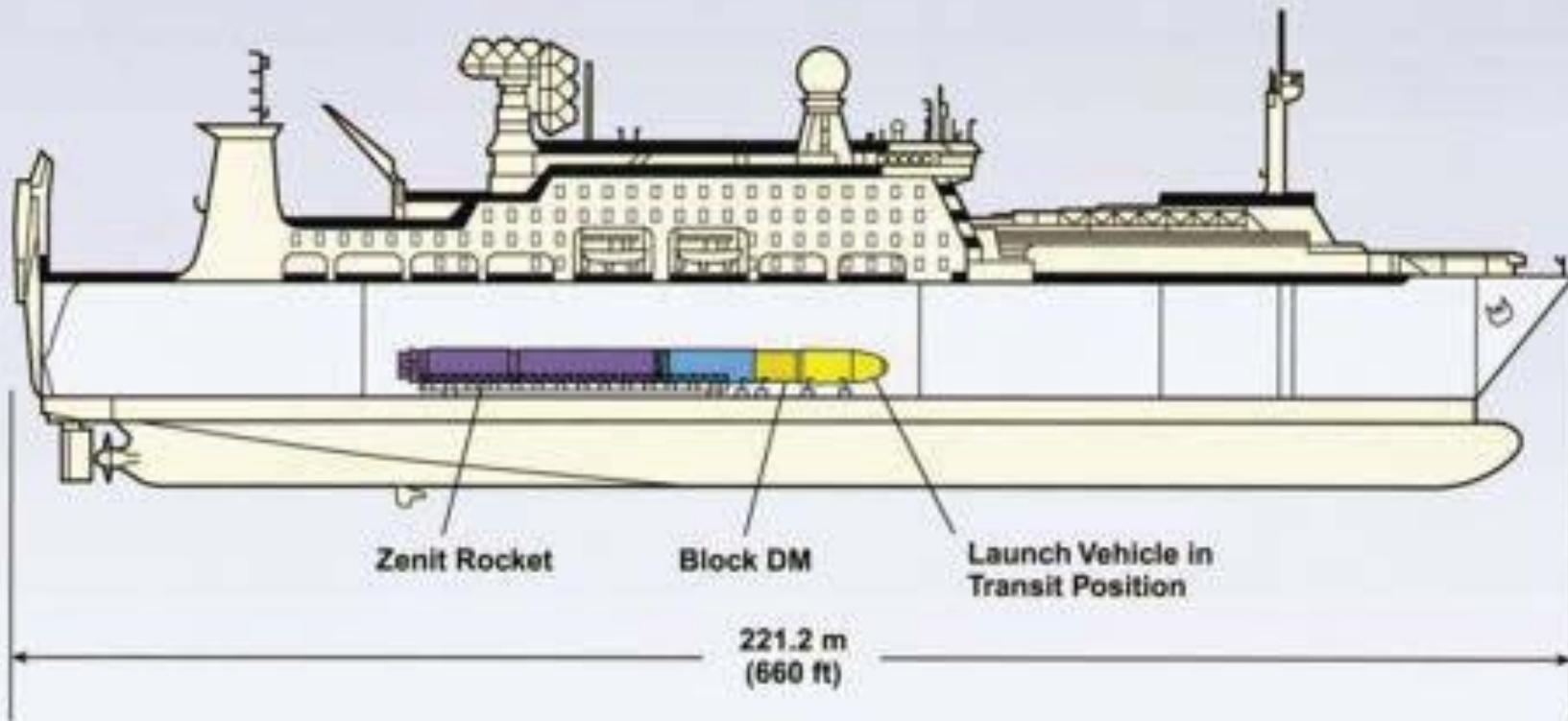
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# Launch Platform



Courtesy of the Sea Launch Company 36

# Assembly and Command Ship



Courtesy of the Sea Launch Company

# Sea Launch Operations



- Integration of rocket stages and payload at home port in Long Beach, CA
- Launches performed from the Equator, 154 degrees west (south of Hawaii)

Courtesy of the Sea Launch Company

Small Team performs ground checkout and launch

	Ground Processing Team	Launch Team*
Americans	80	40
Russians	200	140
Ukrainians	50	50
Norwegians	75	70
<b>Totals</b>	<b>405</b>	<b>300</b>

\* Launch Team is a subset of the Ground Processing Team; Ground Processing team members that are not required to participate in launch at sea are sent back to their companies and are off the Sea Launch payroll

# Lessons Learned from Sea Launch

- Zenit extremely automated launch vehicle
  - Very little interaction with crew during checkout, pre-launch, and flight
- Single string accountability, no duplications of effort (to some extent driven by export compliance restrictions)
- Low operational cost benefited from original design criteria of Zenit
  - Rollout to pad, fuel and launch in 90 minutes
  - Allows very little time for ground or flight crew involvement
  - Imposes requirements for automatic processes

# DESIGN FOR COST EFFECTIVE OPERATION ONLY PARTLY SUCCESSFUL

- ATTEMPT TO DEVELOP “STRETCH GOALS”
- TIGHT ORION MASS/ARES PERFORMANCE ISSUE INHIBITED IMPLEMENTATION OF OPERATIONAL FEATURES
- NASA DOES NOT HAVE DESIGN-FOR-OPERATIONS ADVOCACY WITH STRENGTH EQUAL TO OTHER TECHNICAL DISCIPLINES
- OPERABILITY MUST BE ADDRESSED MORE VIGOROUSLY TO ENSURE VIABILITY OF THE VISION

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# Structural and Ascent Performance Margin Management

## Problem

- Unrealistic ascent performance requirements eliminated the possibility of effective margin management
  - DOD insisted on 32K lbs polar orbit capability
    - Equivalent to 65K lbs due East
  - NASA needed DOD support of the Shuttle Program
- Continuous pursuit of the elusive 65K lbs due East ascent capability precluded the possibility of holding back some structural margin to avoid costly redesign changes as Program development matured
- Prior to performance enhancement program the Shuttle had an ascent performance shortfall of ~10K lbs

## Actions Taken

- All priorities were subordinated to the quest for ascent performance
  - Very few features supported effective operations
  - Costly structural modifications to maintain the required factor of safety were made

# Structural and Ascent Performance Margin Management (continued)

## Lesson

- Set realistic ascent performance requirements
  - Hold back some margin to be used for problem areas
- Use factors on “not well understood” environments to protect against costly design modifications as Program knowledge matures
- Transition to operations should be made consistent with vehicle operational capabilities imbedded in the design

# CONSTELLATION ONLY PARTLY BENEFITED FROM SHUTTLE EXPERIENCE

- ORION MASS/ARES PERFORMANCE SHOW VERY TIGHT MARGINS EARLY IN DESIGN CYCLE
- TIGHT MARGINS WILL CONTINUOUSLY BURDEN THE DESIGNERS OF FLIGHT SYSTEMS AS THE DESIGN MATURES
- VIGILANT MANAGEMENT OF MASS AND PERFORMANCE THREATS WILL BE REQUIRED
- STRUCTURAL MARGIN MANAGEMENT IS MORE ROBUST

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# The Painful Reality

- At least 2 critical design flaws existed in Shuttle flight system through design, testing and flight testing
  - Not detected or acknowledged as major problems
- A gap existed between actual and perceived state of vehicle robustness and safety
- Although strong indications were present, neither the design nor the operations team identified the problem

# Avoid Repeating History

- Learn about the past
- Develop and maintain a strong System Engineering & Integration team throughout the program life cycle
- Empower engineering to challenge the Projects and Program on issues of design flaws and interaction between the elements
  - Continuously monitor performance and safety throughout the transition to operations and the operations phase
- Cultivate culture of respect for descending opinions
- Transition to operations should be made consistent with vehicle operational capabilities imbedded in the design

# The Big Lesson

- We were not as smart as we thought we were
- Knowledge capture initiatives are helping – but should be practiced as a “contact sport”
- If we want simple and cost effective operations we must design for operations
  - Shuttle designed for performance and cost
  - Constellation needs more emphasis on design for operations
  - NASA is in control of operations destiny- short window of opportunity